

Prediction of grain size evolution during thermal and thermomechanical treatments at the mesoscopic scale: numerical improvements and industrial examples

24th IFHTSE Congress 2017

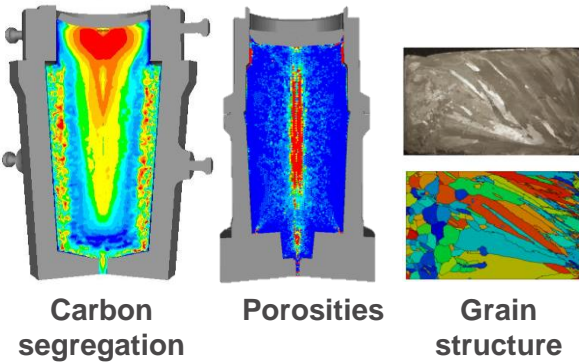
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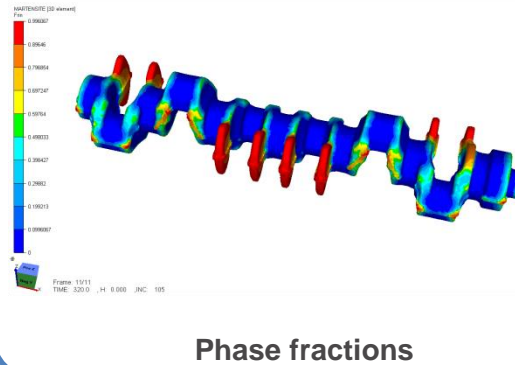
- A growing interest for microstructure modelling throughout the whole process chain...

Solidification



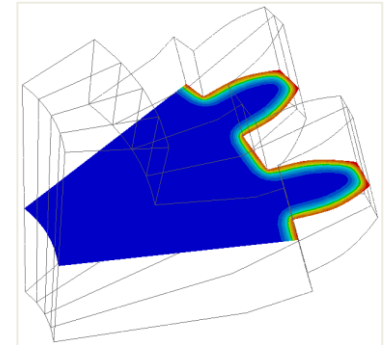
THERCAST®

Heat treatments

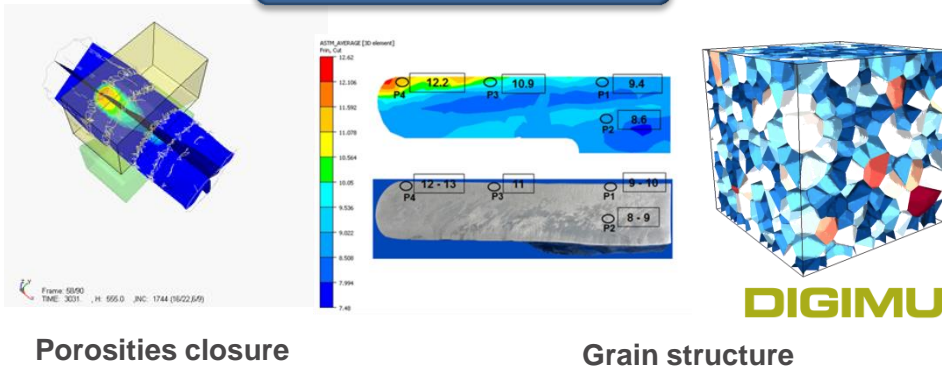


FORGE®

Thermochemical treatments

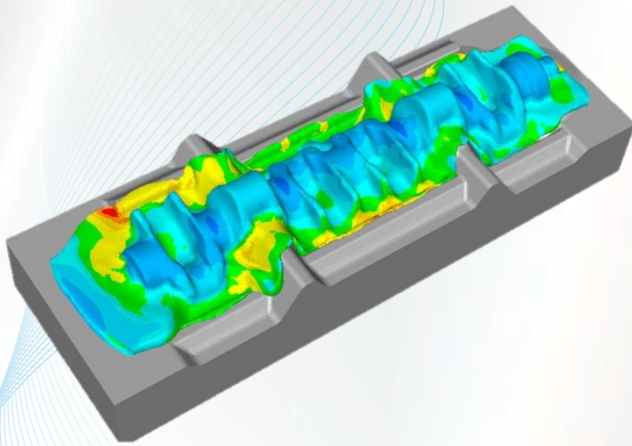


Forming processes

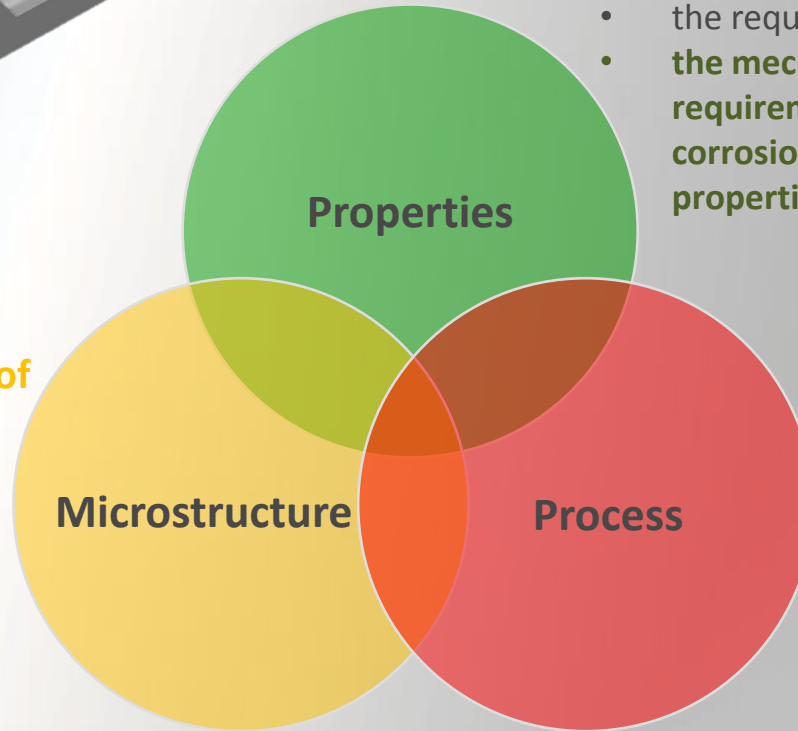


DIGIMU®

- ... and particularly during hot forming processes



Decisive effect of the grain size



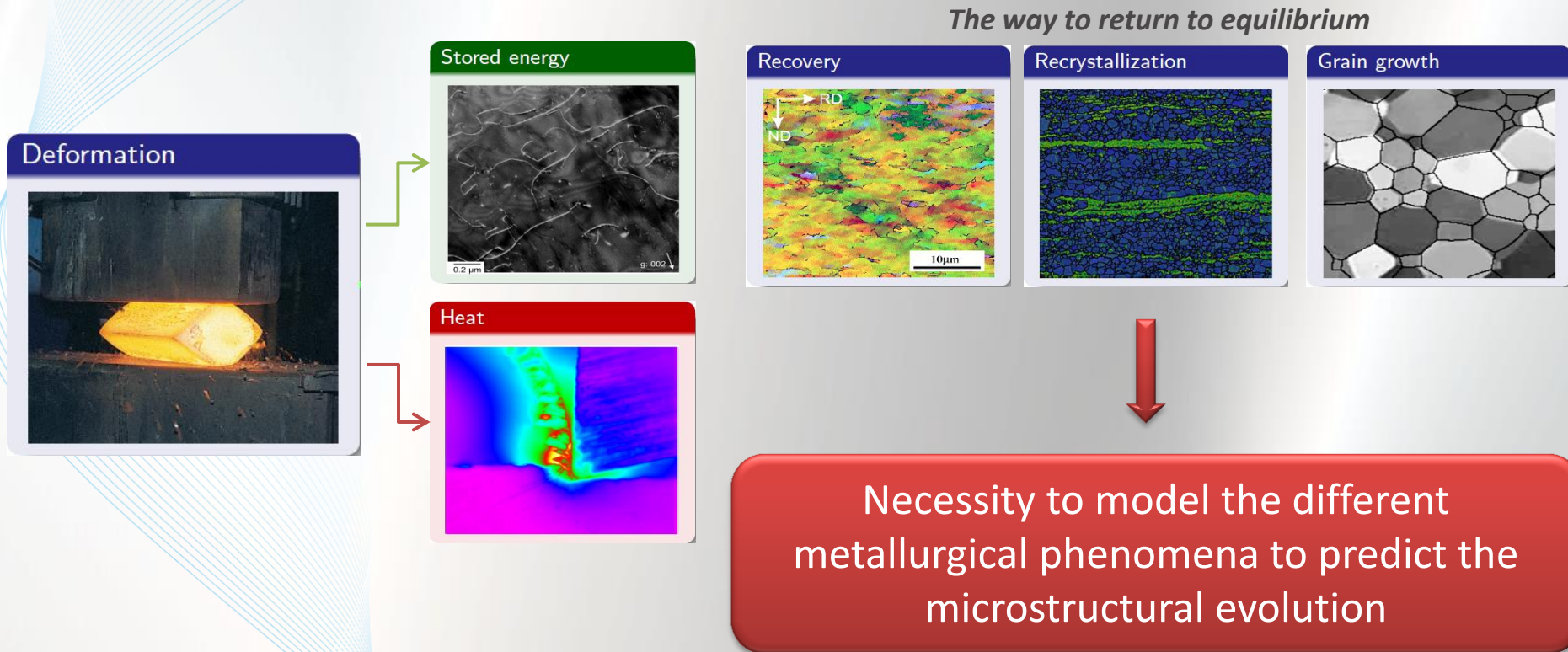
For the parts made, hot forging scheme must ensure:

- the required shape and size
- **the mechanical performance requirements (strength, toughness, corrosion resistance, high-temperature properties...)**

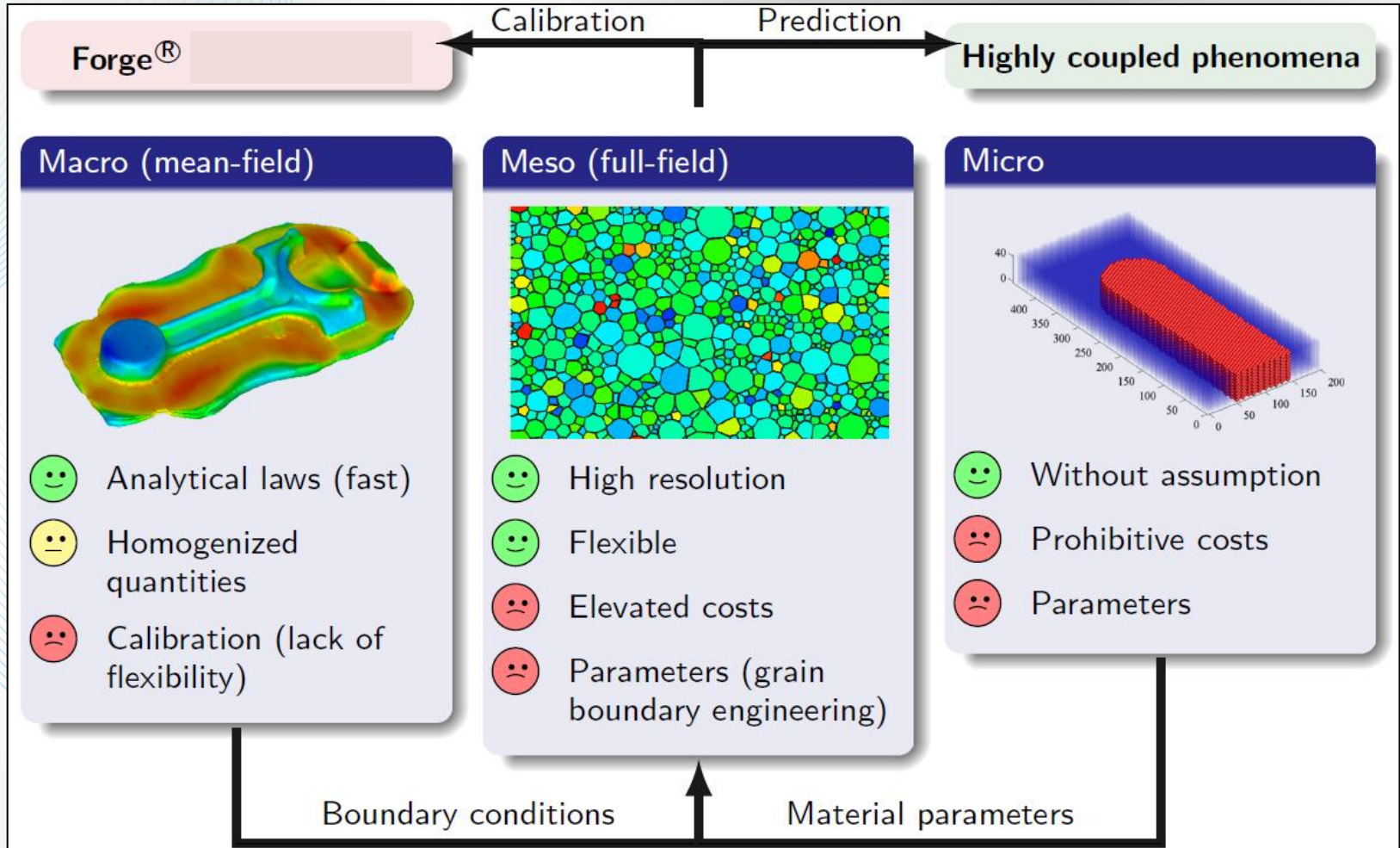
Adapted thermomechanical processing route

Microstructural evolution

- Governed by the process parameters (temperature, strain and strain rate)
- Given by reduction of the internal energy

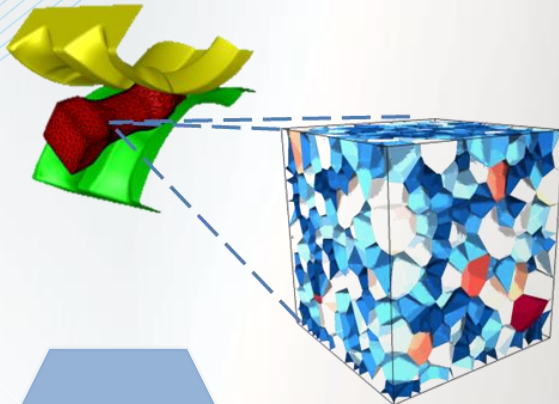


Modelling scales



■ Mesoscale modelling – Full field approach

- Modelling the evolution of the grains (microstructure components fully modelled)
- Simulations performed on Representative Volume Elements (RVE)



Realistic description of microstructural features

- Topological aspects taken into account
- Help for understanding microstructural phenomena
- Modelling local and heterogeneous phenomena



Concept of numerical tests (scale transition)

- Improvement of higher scale models usable for macroscopic simulations
- Calibration of these models



Computation time

- Simulation performed on specific locations of an industrial workpiece (thermomechanical and thermal history as boundary conditions applied to the RVE)



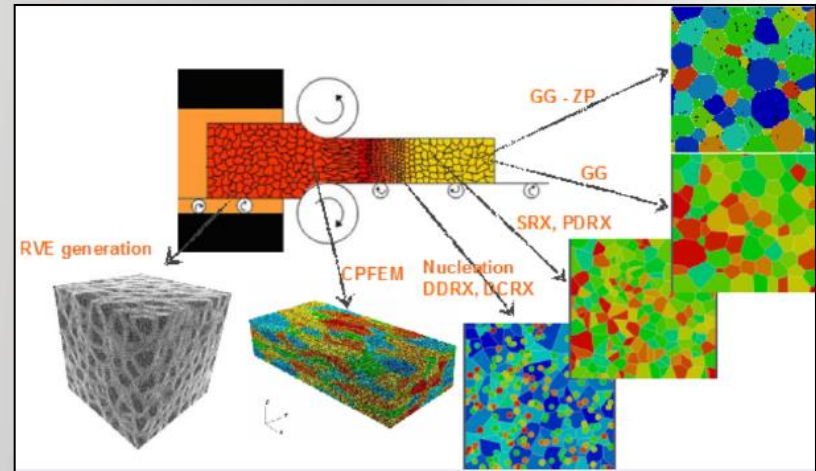
- Context
- Mesoscale modelling in a Level-Set framework
 - DIGIMU®: mesoscale computations in an industrial context
 - Generation of polycrystals in a finite element context
 - Grain boundary migration modelling
 - Numerical improvements
- Application examples
 - Pure grain growth
 - Solutionizing in one-phase field
 - HIP bonding
 - Presence of second phase particles
 - Smith-Zener pinning phenomenon
 - Control of the grain size in an ODS steel
 - Understanding of the abnormal grain growth phenomenon
 - Hot forming processes
- Conclusion

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- From simulations for industry towards simulations by industry

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Development of an industrial solution for simulating microstructural evolutions at the grains scale during thermomechanical processes



Our industrial partners



Digimu - ANR Industrial Chair (2016-2020)



GENERATION OF POLYCRYSTALS IN A FE CONTEXT

Microstructure immersion in a FE mesh

Implicit description of the interfaces using a level-set framework

What is a level-set function?

Signed distance function

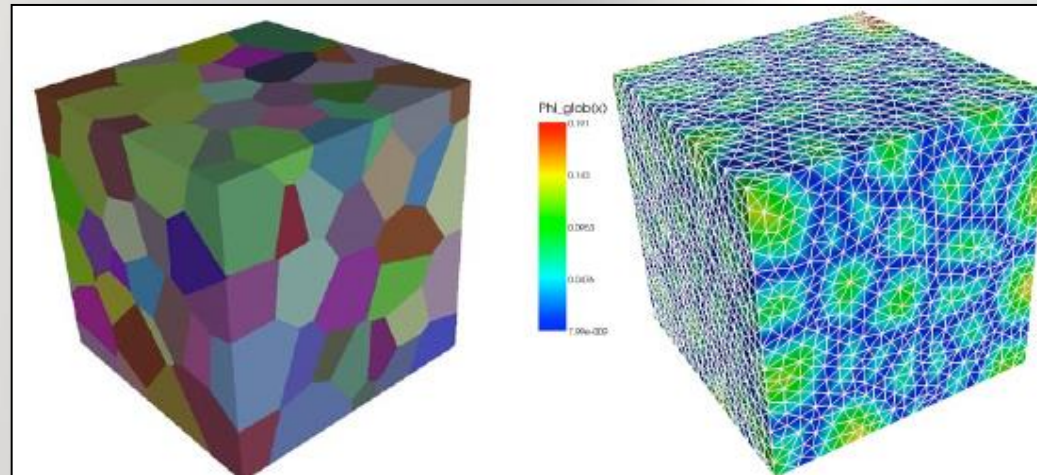
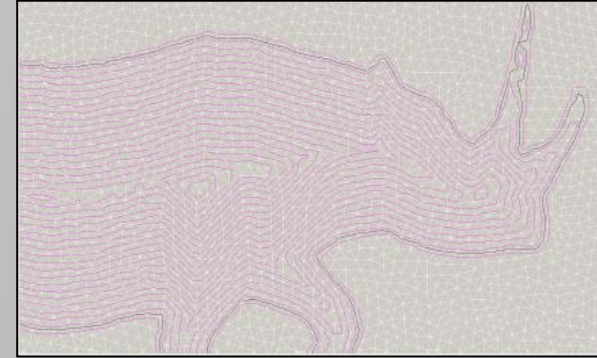
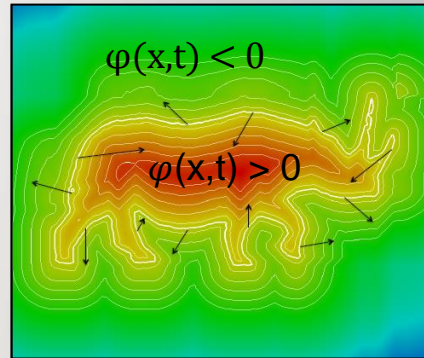
$$\begin{cases} \psi(x, t) = \pm d(x, \Gamma(t)), & x \in \Omega \\ \Gamma(t) = \{x \in \Omega, \psi(x, t) = 0\} \end{cases}$$

Evolving interfaces

Transport of a LS function

$$\begin{cases} \frac{\partial \psi(x, t)}{\partial t} + \vec{v} \cdot \nabla \psi = 0 \\ \psi(x, t = 0) = \psi^0(x) \end{cases}$$

- Immersion of a polycrystal into a FE mesh
 - Statistical random processes (Laguerre Voronoï tessellation)
 - Experimental images
- ➔ Extension to several LS functions



[Bernacki et al., 2008], [Bernacki et al., 2009], [Bernacki et al., 2011], [Fabiano et al. 2014], [Hitti et al. 2012]

GRAIN BOUNDARY MIGRATION MODELLING

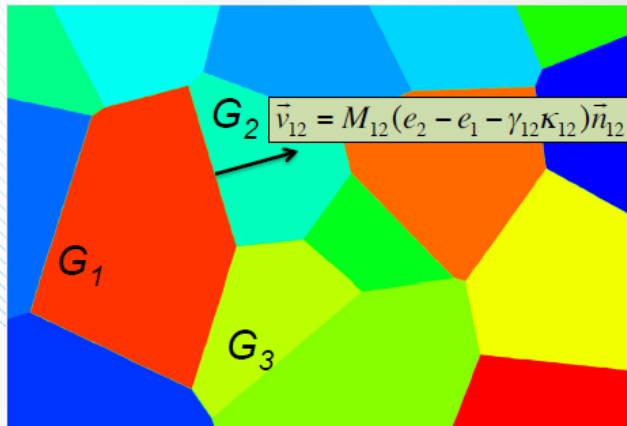
Normal velocity of a grain boundary

$$\vec{v} = m (\tau \Delta \rho - \gamma \kappa) \vec{n}$$

- m : grain boundary mobility
- γ : grain boundary energy
- κ : grain boundary mean curvature
- $\tau \Delta \rho$: stored energy
- \vec{n} : outward normal unit vector

Thermodependent

Driving force for grain boundaries motion



- Convective-diffusive approach

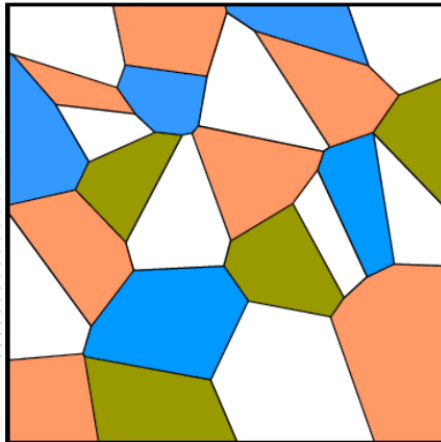
$$\begin{cases} \frac{\partial \psi_i(x, t)}{\partial t} - M \gamma \Delta \psi_i(x, t) + \vec{v}_e \cdot \nabla \psi_i(x, t) = 0, & \forall i \in \{1, \dots, N_p\} \\ \psi_i(x, t = 0) = \psi_i^0(x), \end{cases}$$

$$\vec{v}_e(x) = M \sum_{i=1}^{N_p} \sum_{\substack{j=1 \\ j \neq i}}^{N_p} \chi_i(x) f(\psi_j(x), l) (\mathcal{E}_i(x) - \mathcal{E}_j(x)) \frac{\nabla \psi_j(x)}{\|\nabla \psi_j(x)\|}$$

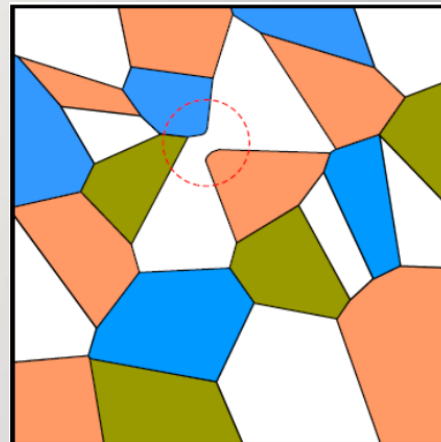
■ How to reduce computation times?

Reduce the number of LS functions

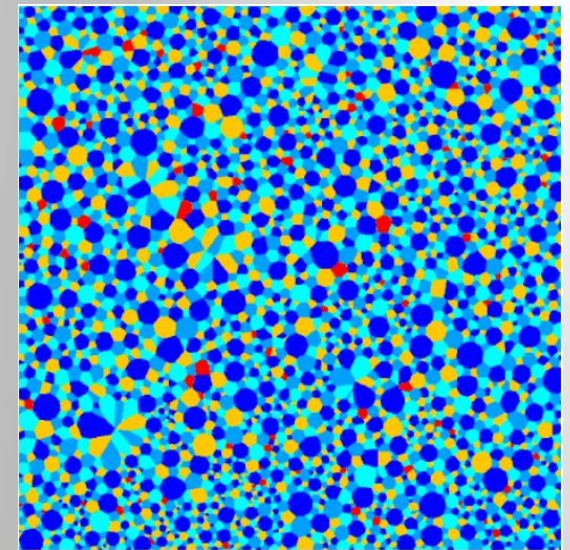
- Use of *Global Level Set functions*: a set of initially distinct grains can be packed in a single LS function
- Associated with evolutive graph coloring technique to avoid numerical coalescence : *Swapping algorithm*



25 grains represented by 4 colors



Coalescence



Microstructure composed of 3680 grains represented by 5 GLS functions

[Scholtes et al. 2015]
[Scholtes et al. 2016a]

How to reduce computation times?

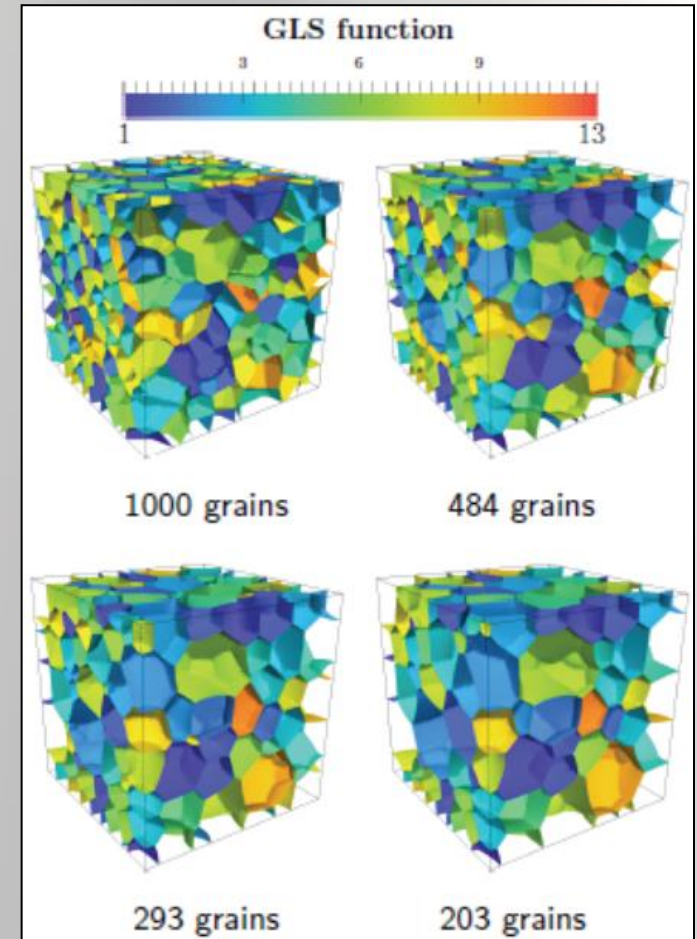
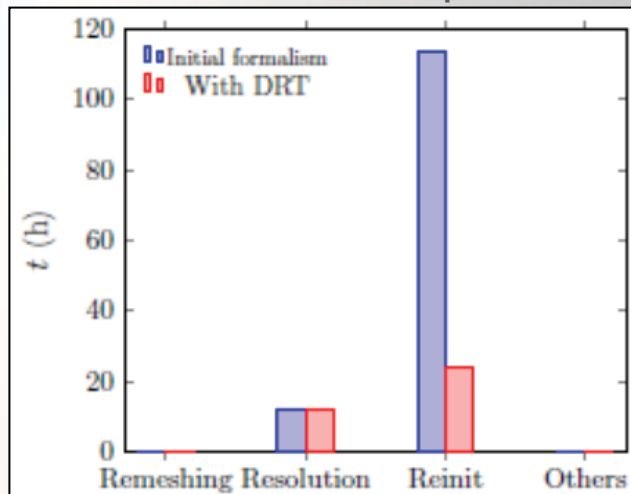
Optimize the main steps of the computation

- Development of a new formalism for the reinitialization procedure*: the *Direct Reinitialization (DR) method*

Example: 3D grain growth case (12CPUs)

- 5h of heat treatment
- Initial polycrystal composed of 1000 grains
- Material : 304L steel

CPU times using the initial formalism or the DR method for the reinitialization procedure



[Shakoor et al., 2015]

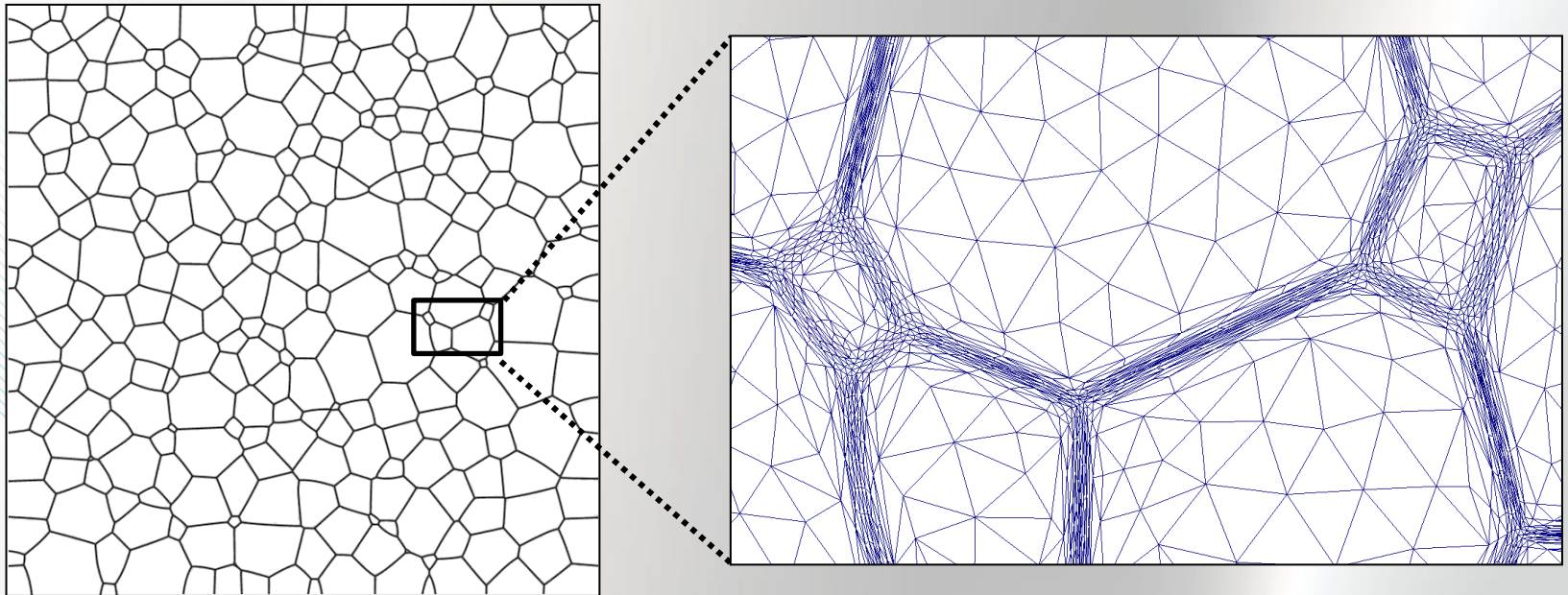
*correction of the LS functions after an increment of computation in order to restore their metric properties

■ How to reduce computation times?

Reduce the number of elements without losing precision

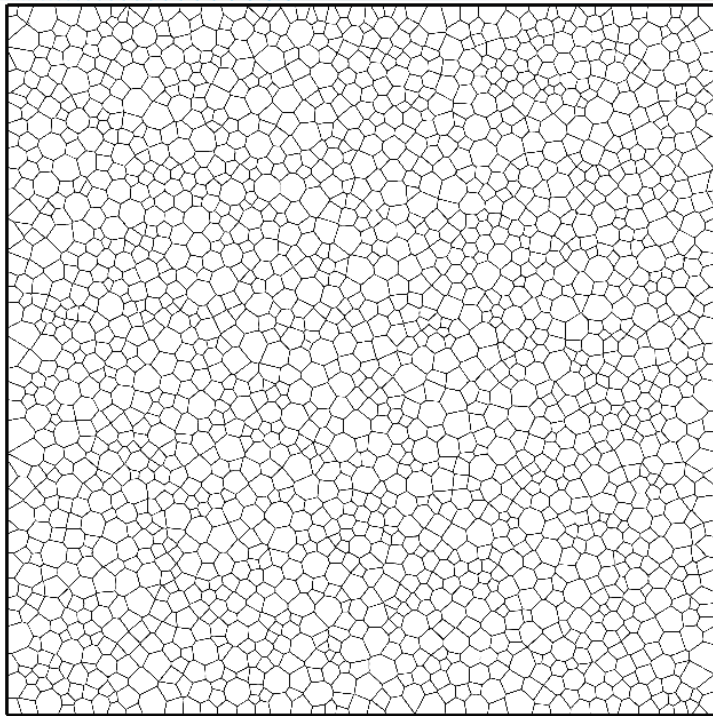
Realistic predictions necessitate a sharp description of the interfaces

- Use of *anisotropic mesh adaptation* (and *periodic remeshing*) around grain boundaries



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■ Solutionizing treatment in the one-phase field



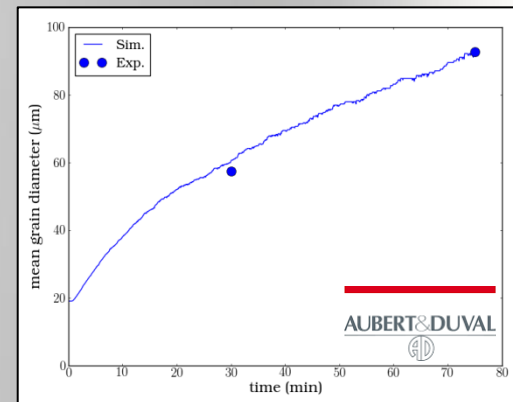
Inconel 718 heat treated 75min at 1040°C
 ($\langle d_0 \rangle = 20\mu\text{m}$, 100% γ phase)

Grain growth in monophasic structures

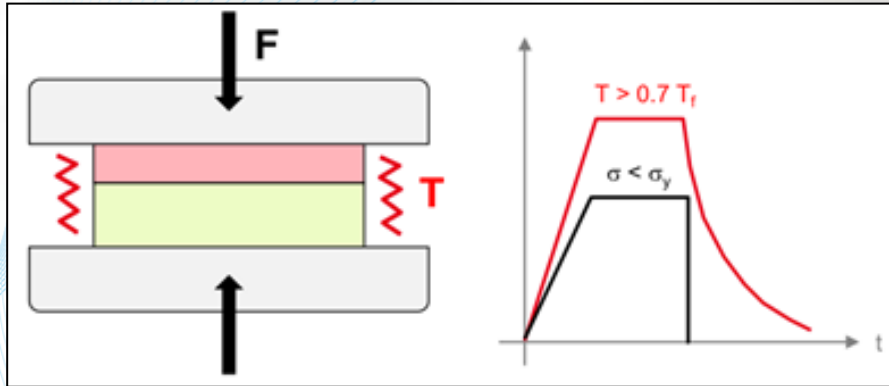
- Microstructural evolution driven by grain boundaries (GB) curvature only (capillarity effect, no stored energy)

$$\begin{cases} \frac{\partial \psi_i(x, t)}{\partial t} - M\gamma\Delta\psi_i(x, t) + \cancel{\bar{v}_i \cdot \nabla \psi_i(x, t)} = 0, & \forall i \in \{1, \dots, N_p\} \\ \psi_i(x, t = 0) = \psi_i^0(x), \end{cases}$$

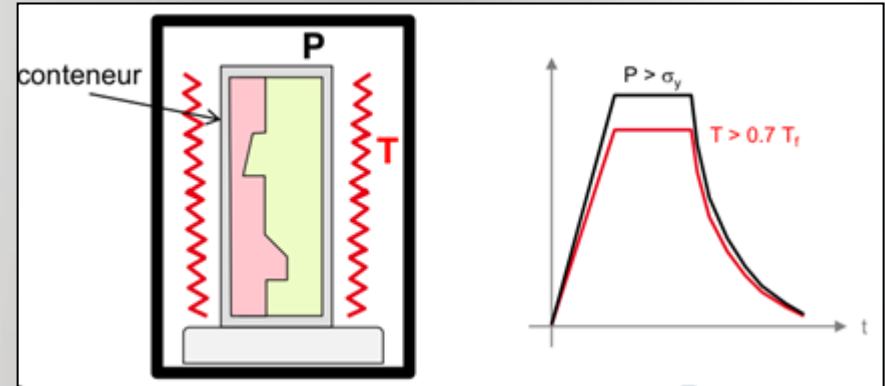
- Uniform GB mobility (thermodependent)
- Uniform and isotropic GB energy
- Influence of initial grain size distribution



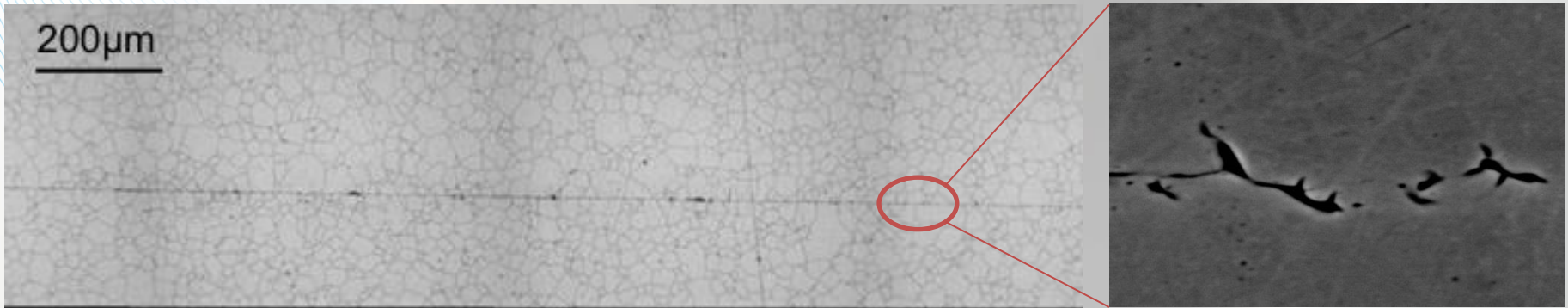
■ HIP bonding



HIP bonding with press

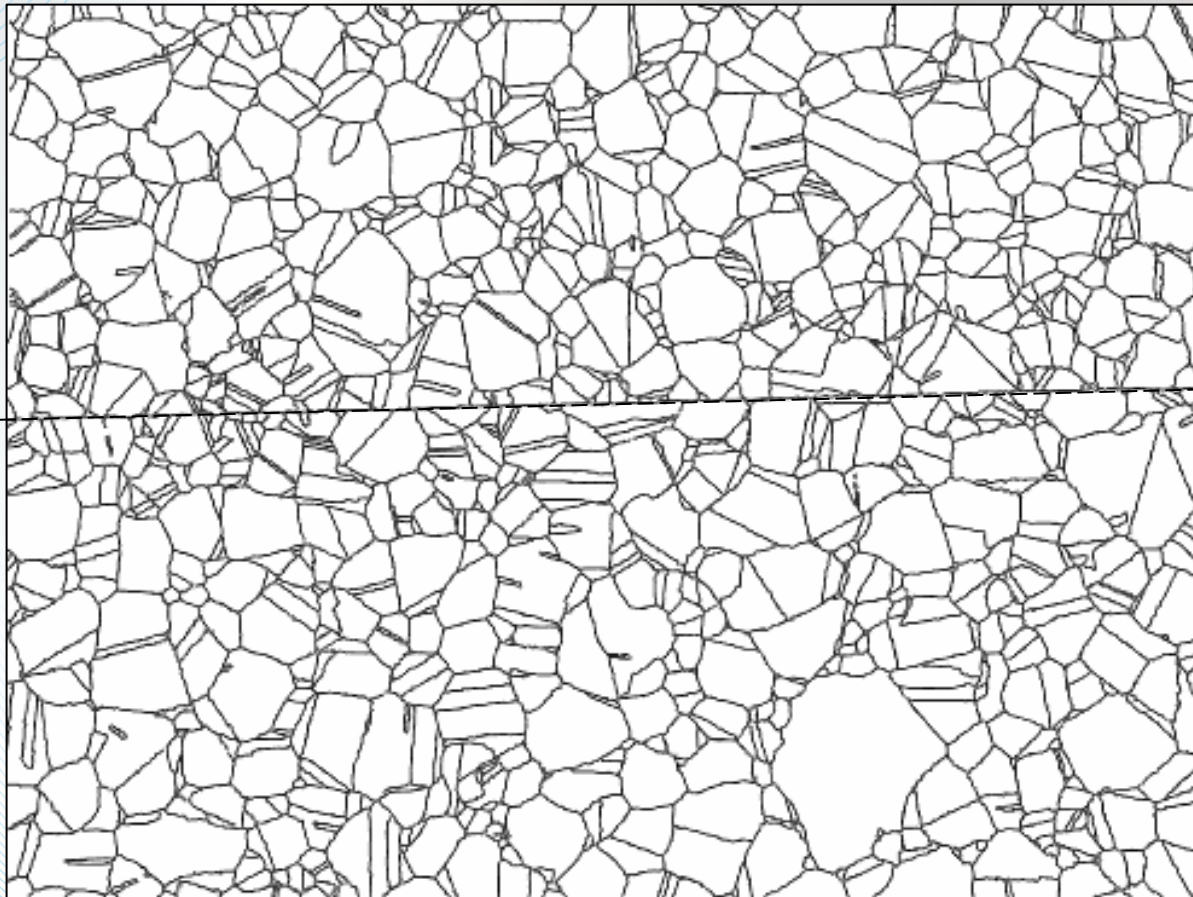


Hot Isostatic Pressing (HIP)

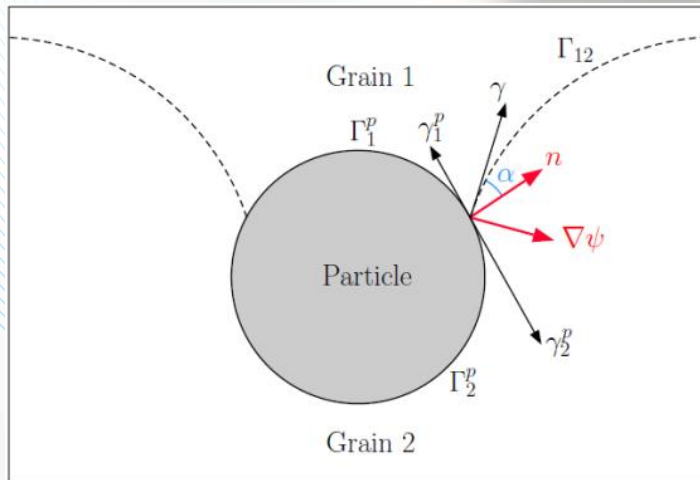
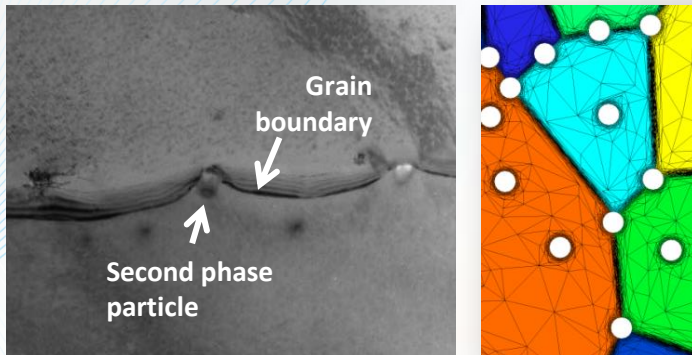


[E. Rigal – CEA Liten]

- HIP bonding



■ Smith-Zener pinning phenomenon



What is particle pinning?

- Dragging force exerted by SPP on GB
 - ➔ *Slow down the GB kinetics*
 - ➔ *Enable to control the final grain size*

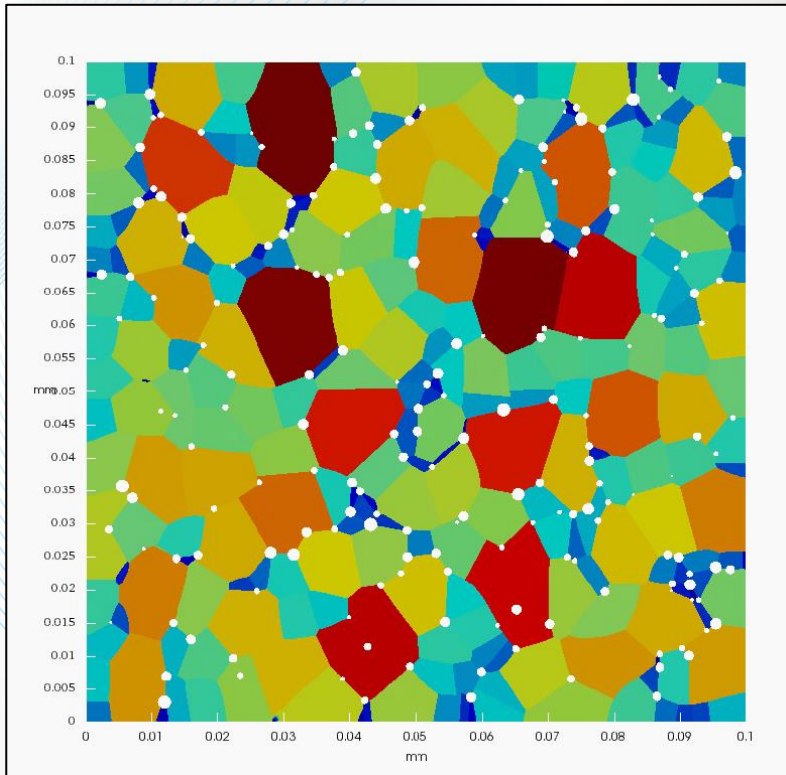
In LS context

- SPP explicitly represented in the FE mesh
 - ➔ *No assumptions concerning the interactions between GB and SPP*
 - ➔ *Coherent or incoherent interfaces can be considered by applying the suitable boundary conditions*

$$\frac{\nabla\psi}{\|\nabla\psi\|} \cdot \vec{n} = \nabla\psi \cdot \vec{n} = \sin(\alpha)$$

[Agnoli et al., 2013], [Agnoli et al., 2014], [Scholtes et al., 2015], [Scholtes et al., 2016b]

Control of the grain size in an ODS steel (Oxide Dispersion Strengthening)

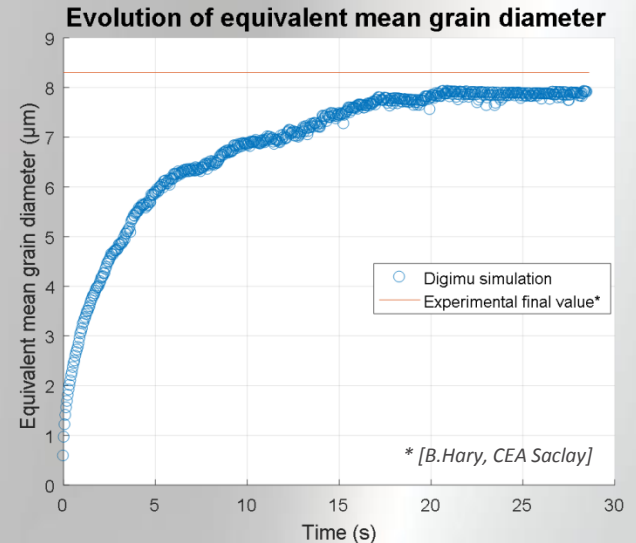


$\langle r_{part} \rangle = 600\text{nm}$
 $f = 2,5\%$

[F. Villaret, B. Hary, Y. de Carlan, T. Baudin, R. Logé, M. Bernacki]



- Ferritic steel + $\text{Y}_2\text{Ti}_2\text{O}_7$ nanoparticles (oxides)
- Dislocations and grain boundaries pinning on the oxides

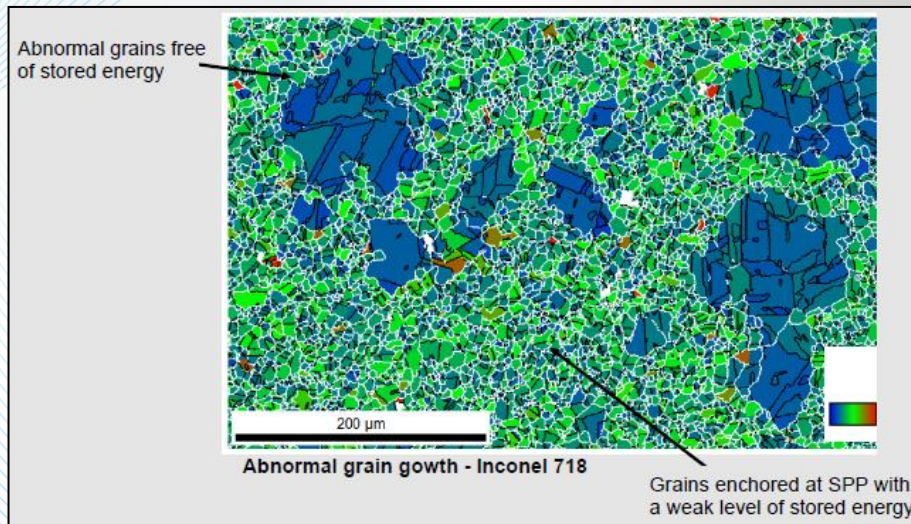


* [B.Hary, CEA Saclay]

APPLICATION EXAMPLES – PRESENCE OF SPP

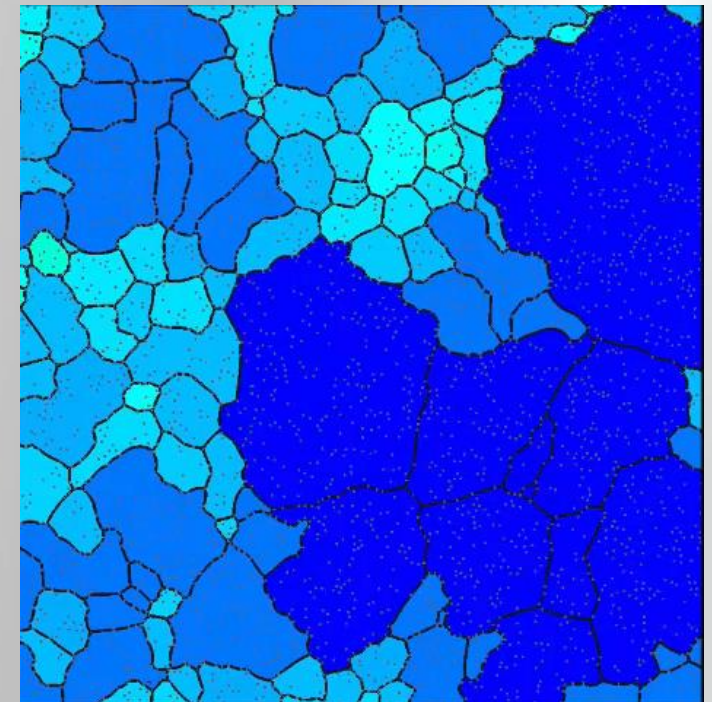
■ Understanding of the abnormal grain growth phenomenon

- Growth of a limited number of grains much faster than the rest
- Decrease of mechanical properties



Phenomenon controlled by the balance of:
capillarity, stored-energy and pinning forces

[Agnoli et al., 2013], [Agnoli et al., 2014]



Local heterogeneity simulated implicitly

Modelling the different physical phenomena

Work hardening

Recovery

Grain boundary migration

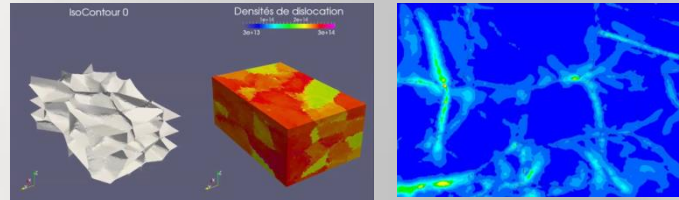
Nucleation of new grains

Precipitation

Two approaches:

- Local scale with Crystal Plasticity Algorithm

 High computational costs for industrial applications



- Macroscopic scale with phenomenological laws

Example: Yoshie Laasraoui Jonas law $\frac{\partial \rho}{\partial \varepsilon} = K_1 - K_2 \rho$ $\frac{\partial \rho}{\partial t} = -K_s \rho$

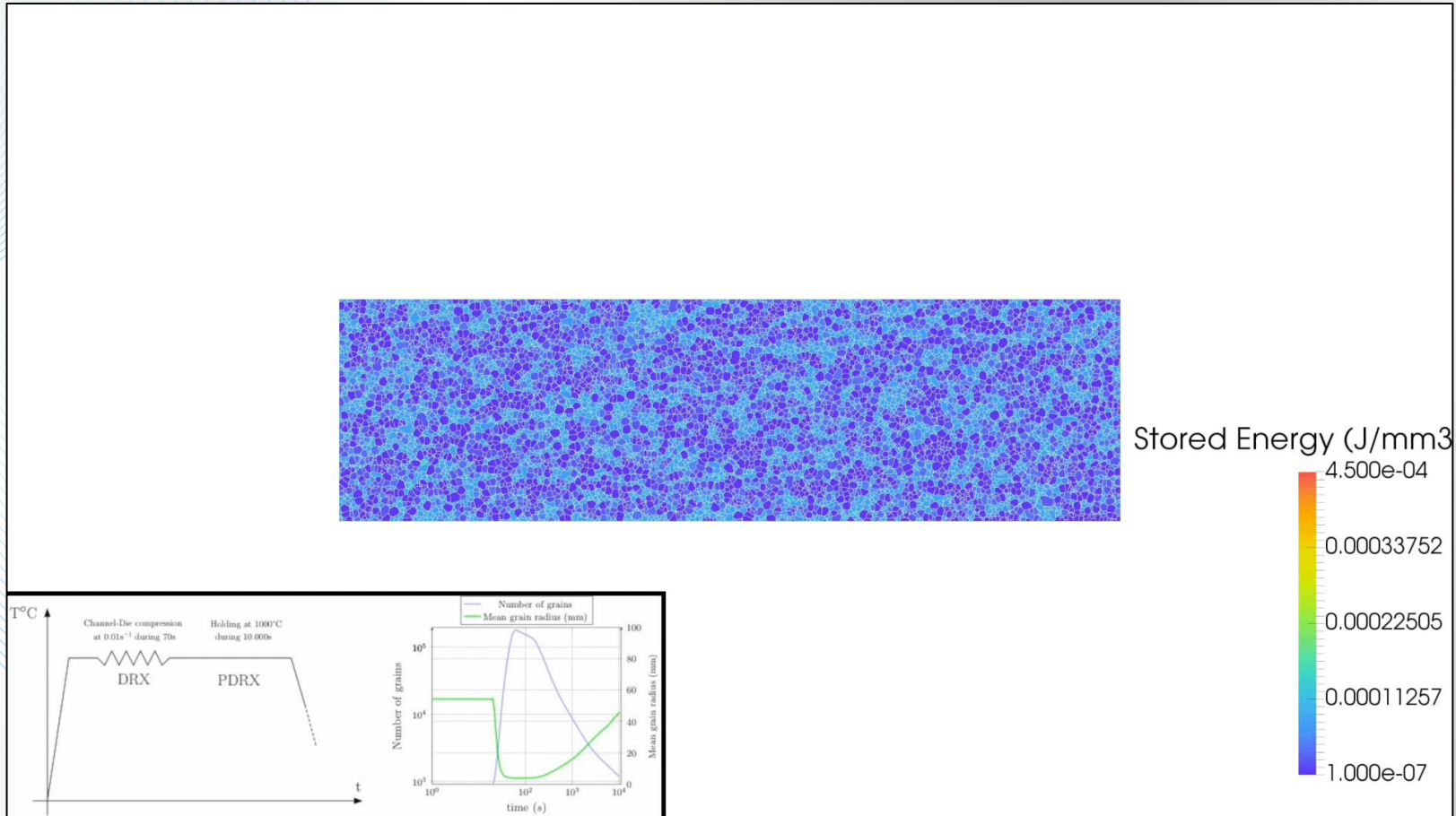
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Calculation of:

- a criterion for nucleation (ρ_{cr})
- a nucleation rate (\dot{N})
- a critical nucleus size (r^*)

[Maire et al., 2017]

Dynamic and Post-dynamic recrystallization



[Maire et al., 2017]

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CONCLUSION & PERSPECTIVES

Prediction of grain sizes evolution during thermomechanical and thermal treatments: a key for optimizing final in-use metal properties

Microstructural evolution modelling at the mesoscopic scale

- Simulate **heterogeneous** and **local** phenomena
- **Improve** mean field models for **macroscale computations**

Approach based on a Level Set description of the interfaces in a finite element framework

- Deterministic approach based on the resolution of convective-diffusive equations of the level set functions
- Grain boundary migration given by the balance of capillarity, stored-energy and pinning forces

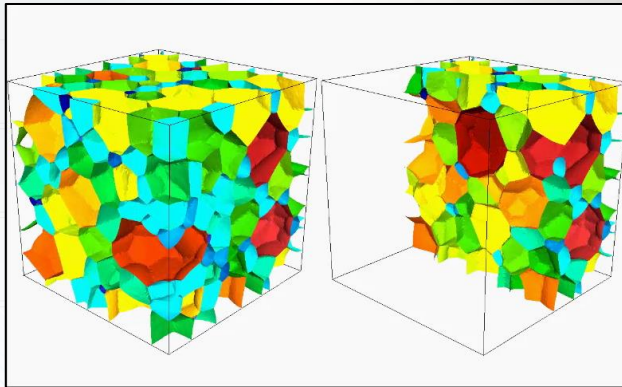
Will to propose an industrial solution

- Numerical improvements done on the method to improve computational efficiency
- Step by step introduction of the developments into the DIGIMU[®] software

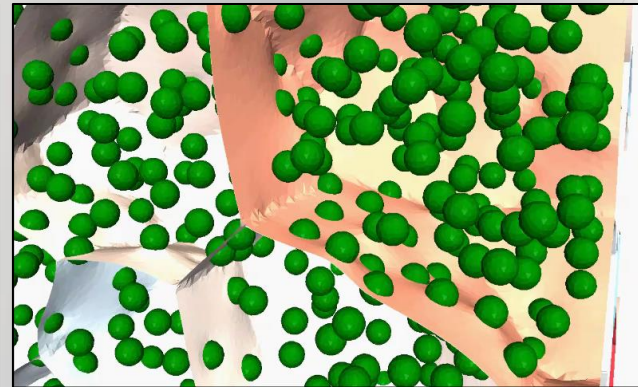
Future developments

- Continuous improvements of the physical models (anisotropy, phase transformations...)
- Towards full 3D simulations: intensive work to reduce computation times

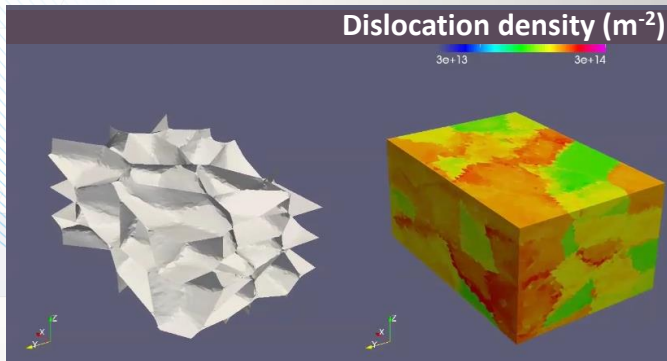
Pure grain growth¹



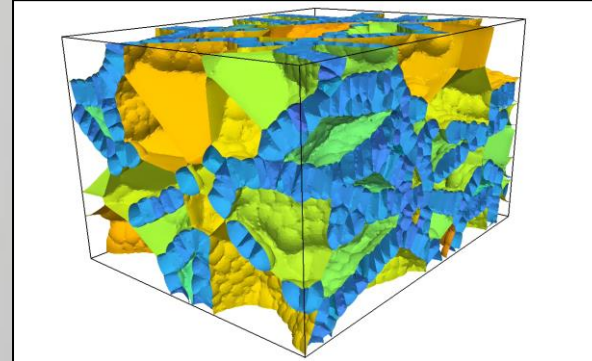
Pinning effect on second phase particles²



Crystal plasticity simulations (CPFEM)³



Dynamic and Post-dynamic recrystallization⁴



¹[Scholtes, 2015]
²[Scholtes, 2016b]
³[Fabiano, 2014]
⁴[Scholtes, 2016a]

- [Scholtes et al. 2016a]** B. Scholtes, R. Boulais-Sinou, A. Settefrati, D. Pino Muñoz, I. Poitault, A. Montouchet, N. Bozzolo, and M. Bernacki. 3D level set modeling of static recrystallization considering stored energy fields. *Computational Materials Science*, 122:57–71, 2016.
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- [Shakoor et al. 2015]** M. Shakoor, B. Scholtes, P.-O. Bouchard, and M. Bernacki. An efficient and parallel level set reinitialization method - application to micromechanics and microstructural evolutions. *Applied Mathematical Modelling*, 39(23-24):7291–7302, 2015.
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- [Bernacki et al. 2009]** M. Bernacki, H. Resk, T. Coupeuz, and R. Logé. Finite element model of primary recrystallization in polycrystalline aggregates using a level set framework. *Modelling and Simulation in Materials Science and Engineering*, 17(6):064006, 2009.
- [Bernacki et al. 2008]** M. Bernacki, Y. Chastel, T. Coupeuz, and R. Logé. Level set framework for the numerical modelling of primary recrystallization in polycrystalline materials. *Scripta Materialia*, 58(12):1129–1132, 2008.
- [Boulais-Sinou et al. 2016]** R. Boulais-Sinou, B. Scholtes, D. Pino Muñoz, C. Moussa, I. Poitault, I. Bobin, Montouchet A., and M. Bernacki. Full field modeling of dynamic recrystallization in a global level set framework, application to 304L stainless steel. *Proceedings of NUMIFORM 2016*, 2016.
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